SOIL INVESTIGATION REPORT

Client: Gujarat Industries Power Company Limited

РМС: -

Design Consultant: -

EPC: -.

Project: Geotechnical Investigation for proposed Solar		Riv.:
plant at Surat Lignite Power Plant, Village: Nani Naroli,	2122222	0
Tal: Mangrol, Dist: Surat.		

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Notes:

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			Prepar	ed	Approv	ved

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Annexure:

- Field & Laboratory Test Results
 Summary of Geotechnical Exploration

ABSTRACT

In the following pages, is presented the report with analysis, prepared from the thorough study of geotechnical investigation results.

The detailed scope of work was decided after the discussion with client. The test location detail is shown in layout plan submitted with report.

A complete geotechnical investigation work was undertaken to obtain the required subsurface information to study and define the nature and behavior of soil. Such information was obtained through following steps:

- > By making test bores and other field tests.
- By observing ground water table in boreholes
- By performing required in-situ tests
- By testing the soil in laboratory to classify it and to determine the engineering properties of soil.

DISCLAIMER

We have employed accepted geotechnical engineering procedures and our opinions and conclusions are made in accordance with generally accepted principles and practices of these professions. The contents of this report are valid as of the date of preparation. However, changes in the condition of the site can occur over time as a result or either natural processes or human activity. In addition, advancements in the practice of geotechnical engineering, engineering and changes in applicable practice codes may affect the validity of this report. Consequently, this report should not be relied upon after an elapsed period of 12 months without a review by this firm for verification of validity. Our investigation did not include the evaluation or assessment of any potential environmental hazards or groundwater contamination that may be present. Soil being a heterogeneous material, any deviation in soil strata encountered after foundation excavation shall refer to us for further consultation.

1.0 INTRODUCTION:

Gujarat Industries Power Company Limited appointed M/s Unique Engineering Testing & Advisory Services as Geotechnical Investigating Agency for above mentioned Project.

1.1 PROJECT DESCRIPTION:

The proposed site is located at Surat Lignite Power Plant, Village: Nani Naroli, Tal: Mangrol, Dist: Surat. It is a construction project of Solar plant.

2.0 SCOPE OF WORK:

The principal objective of the exploration work was to determine the soil profile and to provide foundation recommendation.

The entire field testing was carried out as per relevant IS codes and/or as per the instructions of the representatives of the clients. The samples collected from various test locations, were sealed, labelled and transported to our laboratory at Udhna, Surat. The required laboratory tests were conducted as per relevant IS codes.

This report has been prepared after careful study of the field and laboratory test results.

2.1 FIELD TESTS PERFORMED:

- Drilling 6 no. of 150 mm dia. bore hole with casing whenever required up to maximum depth of 15.0 m from ground level or hard strata.
- Carry out Standard penetration Test (SPT) at every 1.0/1.5 m interval alternate to undisturbed sampling or continuous SPT at 1.0/1.5 m depending on cohesive & non-cohesive formation.
- Collecting disturbed soil sample at every meter interval or as per the stratification of soil and recording depth at which soil changes.
- Collecting undisturbed samples (UDS) at 1.0/1.5 m interval alternate to S P Test.
- Observation of ground water table using drilled holes.
- Conducting 2 Nos. of Electrical Resistivity Test
- Excavating 2 Nos. of Trail Pits.

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2.2 LABORATORY TEST PERFORMED:

- Natural moisture content.
- Field Density, Moisture content and Dry Density of undisturbed samples.
- Grain size Analysis of SPT samples, UD samples and disturbed samples covering each soil strata.
- Atterburg's Limit for samples as per above. (LL, PL, SL)
- Specific gravity Test for Undisturbed samples.
- Diff. Free Swell Index/Swelling Pressure Test
- Consolidation Test
- Modified Proctor Test
- Soak CBR Test
- Test for shear properties of selected samples.
 - a) Unconfined compressive Strength on saturated cohesive soils.
 - b) Triaxial Shear Test/Direct Shear Test (As per soil condition) under UU condition without Pore pressure measurement as per in situ conditions. Normally Soft cohesive saturated samples will be consolidated at average Overburden pressure.

2.3 DRILLING:

Drilling of 150 mm ϕ borehole is carried out by manual shell & auger boring method/mechanical rotary drilling machine. Care is taken before conducting S P Test or Collecting U D Samples that the bore is cleaned properly.

Casing is required to be lowered if the boreholes do not retain its shape. Care is taken that ground water level is maintained during the drilling and particularly before testing or sampling levels. In no case casing was allowed to advance below the bottom of borehole.

2.4 STANDARD PENETRATION TEST:

The Standard Penetration Tests are carried out as per I. S. 2131: 1981. In general, the tests are conducted at 1.0/1.5 m interval alternate to the undisturbed sampling or as dictated by existing soil strata.

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Before testing, the borehole is cleaned properly, and Split Spoon Sampler is centrally seated in borehole. In case of SPT to be conducted below water table care is taken that casing position is above the borehole depth. The water level in borehole is maintained above or at least at the water table.

A standard hammer (Donut type) of 63.5 kg is dropped from a height of 75 cm. and the no. of blows for penetration of Split Spoon Sampler for 0-15, 15-30 and 30-45 cms are noted. Standard Penetration Test Value N_s is considered for 15-45 cms penetration values. Sample for moisture content is collected in moisture cans. For non-plastic silts and fine Sands N_s value is corrected for effective overburden pressure and dilatancy Correction is added for tests conducted below water table.

2.5 DISTURBED AND UNDISTURBED SAMPLES:

Disturbed samples from shell or from Split Spoon Sampler is collected in polythene bags with proper labels.

Undisturbed samples in 70 mm ϕ Shelby tubes are collected alternate to Standard Penetration Test at 1.5 m. interval. The sampling tube is connected to the rod adopter with ball check valve. Before lowering the sampler, the bore is cleaned properly, and sampling tube is lightly oiled from inner and outer side.

Sampling tube is pushed into the borehole by pressure hammering as per the soil stiffness. The sampling tube is immediately waxed after covering with aluminum foil.

In case of medium to coarse, non-cohesive, sand samples, where sampling is unsuccessful, Standard Penetration Test is carried out on cleaning the borehole.

2.6 LABORATORY TEST:

Disturbed, undisturbed and S P Test samples from the filed are brought to the laboratory with care and are grouped according to observations in the fields. On completion of shear, compressibility, permeability etc. tests on U D samples, these samples are placed in oven along with the S P Test samples and disturbed samples. Samples are selected such that each soil strata is adequately represented by the physical properties. The representative samples are dried in oven for 24 hours at 110 ± 5 °C.

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2.6.1 PHYSICAL PROPERTIES:

The moisture cans collected from S P T samples from the field are weighed and placed in oven for drying to determine natural moisture content (NMC).

U D samples are extracted using extractor and samples are prepared as per the required sizes of the test to be performed. Before extracting from tube, weight and volume of sample are noted. Average bulk density is calculated in laboratory and samples are placed in oven to get the field moisture content for computing the dry density.

Specific gravity with specific gravity bottle / pycknometer is calculated as per I. S. 2720 (part -3, section 1&2): 1980. From the results of dry density and specific gravity the saturation of sample in % is calculated which is a useful data for deciding the condition of triaxial shear test

Grain size analysis is made by I. S. sieves. I.S sieves commonly used are 4.75 mm, 2.00 mm, 1.00 mm 425 microns, 250 microns and 75 microns. For the coarse grain soil a graph of partial size v/s cumulative % finer is plotted. For fine grain soil wet analysis is made and material fine than 75 microns is found out by hydrometer test. Mechanical digital single pan balance of 1 kg capacity with 0.1 gram least count is used.

Liquid limits and Plastic limits tests are carried out with distilled water as per I. S. 2720 (part - 5): 1985. The samples are tested at a minimum of 24 hours after the addition of water. For liquid limit test cone penetration method is adopted but occasionally value is checked on Casagrande standard.

For the foundation soil sample showing high plasticity are checked for swelling and shrinkage. Firstly for rough estimate, free swell test as per I. S. 2720 (part – 40): 1977 is being carried out and getting positive indication of swelling. Shrinkage limit test is carried out as per I. S. 2720 (part – 6): 1972.

2.6.2 SHEAR PROPERTIES:

Shear tests are carried out by three methods.

 Unconfined compressive strength as per I. S. 2720 (part – 10): 1973 for the saturated plastic soil undisturbed samples and cores of SPT samples.

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2) Triaxial shear test is carried out on sample size of 38 mm ϕ and 76 mm in height on motorized 30-speed load frame with digital display arrangements for load and porepressure. The confining pressure σ_3 is applied to the cell by oil-water constant pressure system. The test is carried out for Unconsolidated Undrained (UU) test without porepressure measurement as per I.S. 2720 (part – 11): 1971.

The graph for triaxial shear test is plotted by modified method where X-axis represents $\frac{1}{2}(\sigma_1 + \sigma_3)$ and Y-axis represents $\frac{1}{2}(\sigma_1 - \sigma_3)$.

3.0 FOUNDATION RECOMMENDATION:

- Standing water or groundwater was not encountered till termination depth below ground level in BH-01 to BH-06 during the subsurface exploratory boreholes in January 2022. It should be noted that groundwater levels might change and can vary with seasonal rainfall patterns, long-term climate fluctuations and with the influence of local site conditions.
- Three boreholes (BH-1, BH-2 & BH-3) were conducted on virgin soil and three boreholes (BH-4, BH-5 & BH-6) were conducted on filled up soil. This filling is done with fairly uniform nature of soil but have varying stiffness.
- 3. Soil strata are as described in "Summary of Geotechnical Exploration" of this report.

For BH-01, predominantly soil strata are reddish stiff high plastic clay with sand followed by reddish very stiff plastic clayey sand with gravel to reddish very stiff high plastic clay with sand.

For BH-02, predominantly soil strata are brownish silt with medium to coarse sand and gravel followed by yellow very stiff plastic clayey sand to reddish hard high plastic clay with sand.

For BH-03, predominantly soil strata are yellow sandy gravel (highly weathered rock) followed by yellow dense silty medium to coarse sand with boulders to boulders. Strata thereafter are yellow cemented high plastic clay with sand.

For BH-04, neglecting top filling predominantly soil strata are black stiff high plastic clay with sand followed by reddish stiff high plastic clay with sand to black stiff high plastic clay. For BH-05, neglecting top filling predominantly soil strata are reddish stiff high plastic clay followed by black very stiff high plastic clay with sand to yellowish stiff high plastic clay.

For BH-06, neglecting top filling predominantly soil strata are yellow firm high plastic clay with sand followed by black stiff high plastic clay with sand to reddish yellow stiff to very stiff high plastic clay with sand.

- 4. Top 4.0 m soil has high swelling potential in BH-01 & 06. Depth 2.0 m to 3.0 m soil has high swelling potential in BH-02. Depth 1.0 m to 2.0 m soil has high swelling potential in BH-03. Top 1.0 m and depth 2 m to 3 m soil has high swelling potential in BH-04. It shall not be used for back-filling purposes without treatment.
- For both the location shallow foundation proposed at 2.5 m or below from NGL. As per client's request, bearing capacity calculation provided for foundation depth above 2.5 m.
- 6. For foundation resting on soil having high swelling potential (Up to 3 m depth), the pit shall be excavated up to foundation level + 500 mm below existing ground level and shall be backfilled with 500 mm thick compacted selected soil (non-cohesive soil/GSB) in layers. Foundation shall be placed on this compacted modified soil layer. Extent of the selected soil layer shall be 300 mm extra on all sides of the foundation.
- Pile capacity as per suggested load and dia. combination is also given is also given below. Pile capacity shall be confirmed as site by conducting static pile load test as per IS 2911-Part-4.
- 8. IS 3764-1992 shall be followed as a Safety Code for excavation work.

SUMMARY OF ALLOWABLE BEARING CAPACITY CALCULATIONS

1) For BH-01, 02 & 03 (VASTAN SOUTH)-

1.1) For Square Footing –

<u>Design Data :</u>

Foundation Type	: Square Footing
Width of Footing	: 1.00 m to 5.00 m, (increment = 1.00 m)
Depth of Footing	: 1.00 m to 5.00 m, (increment = 1.00 m)
Failure Mode	: General Shear Failure
Shape and Depth Factors	: To be considered
Load inclination	: 0.00 Deg
Water Table	: 1.00 m (Assumed)
Factor of Safety	: 3.00
Permissible Settlement	: 50.00 mm

Soil	From	То	С	Ø	γь	m _v	Е
Strata	(m)	(m)	(Kg/cm ²)	(deg)	(g/cc)	(cm ² /Kg)	(Kg/cm ²)
SC	0.00	3.00	0.30	14.0	1.77	1.54e-02	65.00
SC	3.00	7.50	0.45	16.0	1.80	1.05e-02	95.00
СН	7.50	10.50	1.10	-	1.90	6.70e-03	150.00

Calculations:, Water Table at a depth of 1 m

For General Shear Failure, Ultimate Bearing Capacity is given by

 $\begin{array}{l} q_d = c \; N_c \, s_c \, d_c \, i_c + q \; (N_q - 1) \; s_q \, d_q \, i_q \, + \frac{1}{2} \, B \, \gamma \, N_\gamma \, s_\gamma \, d_\gamma \, i_\gamma \; W' \\ \text{Where} \\ & N_c, \, N_q, \, N_\gamma \; \text{are Bearing Capacity Factors from Table-1 [IS:6403-1981]}, \\ & s_c \,, s_q \,, s_\gamma \; \text{are Shape Factors}, \\ & d_c \,, d_q \,, d_\gamma \; \text{are Depth Factors}, \\ & i_c \,, i_q \,, i_\gamma \; \text{are Inclination Factors}, \\ & c = \text{Cohesion in Kgf/cm}^2, \\ & q = \text{Effective surcharge at base of Fdn in Kgf/cm}^2, \\ & B = \text{Width of Fdn in cms}, \\ & \gamma = \text{Bulk unit weight of foundation soil in Kgf/cm}^3, \\ & W' = \text{Correction factor for location of water table (at a depth of 100 cms)} \end{array}$

<u>Safe Bearing Capacity (Considering a Factor of Safety of 3), is given by :</u> $a_1 a_2 = a_1/3$

 $q_{safe} = q_d / 3$

Immediate Settlement in Cohesive Layer from 0 to 3 m (Si)

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 $= p B (1 - \mu^{2}) I / E$ *Where* $p = Foundation Pressure in Kg/cm^{2}$ B = Width of footing in cm $\mu = Pisson's ratio = 0.5 \text{ for clay}$ I = Influence factor depending on L/B and Ht/B is obtained from Fig 11 [IS 8009 (Part 1)] $E = Young's Modulus of elasticity = 65 Kg/cm^{2}$ Sottlement in Pro Compressed Cohesive L over from 0 to 3 m (St)

Settlement in Pre-Compressed Cohesive Layer from 0 to 3 m (S₁)

 $= \Delta p \times m_{v} \times H$ Where

 Δp = Pressure increment in kg/cm² at a depth 0.75 m below Foundation [obtained from B-1.3 and Fig 17, IS 8009 Part 1]

= p x I_B x number of Influence Areas

 $m_v = \text{Coefficient of volume compressibility} = 0.0154 \text{ cm}^2/\text{kg}$

H = Thickness of compressible stratum from foundation level

Total Settlement

 $S_{f} = S_{i} + S_{1} \\$

Applying Correction for Effect of Depth of Foundation

 $\begin{array}{ll} S_{fd} &= S_f \times \text{Depth Factor} \\ & Where \\ & \text{Depth Factor} = 0.72 \text{ (from Fox's Correction Curves for } \sqrt{(L B) / D} = 1 \text{ and } L / B \\ &= 1 \text{)} \end{array}$

Results of Bearing Capacity

S1	Width	Depth	q safe	Settlement	Remarks
No	(m)	(m)	T/m^2	(mm)	
1	1.00	1.00	19.5	20.7	-
2	1.00	2.00	24.3	26.5	-
3	1.00	3.00	48.0	30.7	-
4	1.00	4.00	56.5	34.0	-
5	1.00	5.00	65.2	36.8	-
6	2.00	1.00	17.5	49.8	q _{safe} reduced for Settlement Criteria
7	2.00	2.00	20.7	42.8	-

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8	2.00	3.00	37.7	49.9	q _{safe} reduced for
9	2.00	4.00	41.3	50.0	Settlement Criteria
10	2.00	5.00	38.2	50.0	
11	3.00	1.00	12.3	49.7	
12	3.00	2.00	16.9	50.0	
13	3.00	3.00	21.8	49.8	
14	3.00	4.00	23.1	49.8	
15	3.00	5.00	25.3	49.8	
16	4.00	1.00	9.9	49.6	
17	4.00	2.00	12.2	49.9	
18	4.00	3.00	15.3	49.9	
19	4.00	4.00	17.0	49.9	
20	4.00	5.00	20.0	49.8	
21	5.00	1.00	8.1	49.8	
22	5.00	2.00	9.9	49.6	
23	5.00	3.00	12.1	49.8	
24	5.00	4.00	14.1	49.8	
25	5.00	5.00	17.2	49.9	

1.2) <u>Summary of Pile Capacity Table For Bored Cast-In Situ Pile – (For Structures)</u>

Pile Dia. in mm	Pile Depth* in m	Axial (Comp.) Capacity in T	Axial (Uplift) Capacity in T	Lateral Capacity in T (Fix Head)	Depth of Fixity in m
400	9	16	14	2.7	4
450	9	19	17	3.5	5
500	9	22	19	4.3	5
600	9	28	24	6.1	6

* From cut-off level.

Note:

a. Cut-off level considered at 1.0 m below EGL.

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Summary of Pile Capacity Table For Bored Cast-In Situ Pile – (For Solar Panel)

Pile Dia. in mm	Pile Depth* in m	Axial (Comp.) Capacity in T	Axial (Uplift) Capacity in T	Lateral Capacity in T (Free Head) – 5 mm deflection	Depth of Fixity in m
	1.5	3	2	0.6	3.0
300	2.0	4	4	0.6	3.0
	3.0	7	6	0.6	3.0

* From cut-off level.

Note:

- a. Cut-off level considered at 0.0 m below EGL.
- b. Top 3 m soil has high swelling potential. Designer should check for this aspect. Pile capacities provided as per client's requirement.

2) For BH-04, 05 & 06 (VASTAN)-

2.1) For Square Footing –

Design Data :

Foundation Type	: Square Footing
Width of Footing	: 1.00 m to 5.00 m, (increment = 1.00 m)
Depth of Footing	: 1.00 m to 5.00 m, (increment = 1.00 m)
Failure Mode	: Local Shear Failure (Considering filled-up soil)
Shape and Depth Factors	: To be considered
Load inclination	: 0.00 Deg
Water Table	: 1.00 m (Assumed)
Factor of Safety	: 3.00
Permissible Settlement	: 50.00 mm

Soil	From	То	С	Ø	γь	m _v	E
Strata	(m)	(m)	(Kg/cm ²)	(deg)	(g/cc)		
СН	0.00	4.00	0.60	-	1.78	2.00e-02	50.00

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СН	4.00	10.00	0.77	-	1.80	1.25e-02	80.00
СН	10.00	15.00	0.90	-	1.90	7.10e-03	140.00

Calculations :, Water Table at a depth of 1 m

For Local Shear Failure, Ultimate Bearing Capacity is given by $q_d = \frac{2}{3} c N'_c s_c d_c i_c + q (N'_q - 1) s_q d_q i_q + \frac{1}{2} B \gamma N'_\gamma s_\gamma d_\gamma i_\gamma W'$ Where N'_c, N'_q, N'_{γ} are Bearing Capacity Factors from Table-1 [IS:6403-1981], s_c , s_q , s_γ are Shape Factors, d_c , d_q , d_γ are Depth Factors, i_c , i_q , i_γ are Inclination Factors, $c = Cohesion in Kgf/cm^2$, q = Effective surcharge at base of Fdn in Kgf/cm², B = Width of Fdn in cms, γ = Bulk unit weight of foundation soil in Kgf/cm³, W' = Correction factor for location of water table (at a depth of 100 cms)Safe Bearing Capacity (Considering a Factor of Safety of 3), is given by : $q_{safe} = q_d / 3$ Immediate Settlement in Cohesive Layer from 0 to 4 m (S_i) $= p B (1 - \mu^2) I / E$ Where p = Foundation Pressure in Kg/cm² B = Width of footing in cm μ = Pisson's ratio = 0.5 for clay I = Influence factor depending on L/B and H_t/B is obtained from Fig 11 [IS 8009 (Part 1)] E = Young's Modulus of elasticity = 50 Kg/cm² Settlement in Pre-Compressed Cohesive Layer from 0 to $4 \text{ m}(S_1)$ $= \Delta \mathbf{p} \times \mathbf{m}_{\mathbf{v}} \times \mathbf{H}$ Where Δp = Pressure increment in kg/cm² at a depth 0.75 m below Foundation [obtained from B-1.3 and Fig 17, IS 8009 Part 1] = p x I_B x number of Influence Areas m_v = Coefficient of volume compressibility = 0.02 cm²/kg H = Thickness of compressible stratum from foundation level

Total Settlement

$S_{\rm f}=S_i+S_1$

= 1)

 $\frac{Applying \ Correction \ for \ Effect \ of \ Depth \ of \ Foundation}{S_{fd}} = S_f \times Depth \ Factor$

Where

Depth Factor = 0.72 (from Fox's Correction Curves for $\sqrt{(L B)} / D = 1$ and L /B

Results of Bearing Capacity

Sl	Width	Depth	q safe	Settlement	Remarks
No	(m)	(m)	T/m ²	(mm)	
1	1.00	1.00	10.7	15.4	-
2	1.00	2.00	12.5	14.7	-
3	1.00	3.00	14.3	18.8	-
4	1.00	4.00	20.6	15.5	-
5	1.00	5.00	22.9	16.7	-
6	2.00	1.00	9.8	35.9	-
7	2.00	2.00	10.7	33.7	-
8	2.00	3.00	11.6	27.8	-
9	2.00	4.00	16.0	24.7	-
10	2.00	5.00	17.2	25.0	-
11	3.00	1.00	8.6	49.5	q _{safe} reduced for Settlement Criteria
12	3.00	2.00	10.1	46.9	-
13	3.00	3.00	10.7	36.7	-
14	3.00	4.00	14.5	34.8	-
15	3.00	5.00	15.2	33.7	-
16	4.00	1.00	6.8	49.4	q _{safe} reduced for
17	4.00	2.00	8.5	49.7	Settlement Criteria
18	4.00	3.00	10.3	45.3	-
19	4.00	4.00	13.7	49.8	-
20	4.00	5.00	14.3	49.6	-

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21	5.00	1.00	5.8	49.4	q _{safe} reduced for
22	5.00	2.00	7.1	49.4	Settlement Criteria
23	5.00	3.00	8.4	49.6	
24	5.00	4.00	10.3	49.7	
25	5.00	5.00	11.1	49.9	

2.2) <u>Summary Of Pile Capacity Table For Bored Cast-In Situ Pile –(For Structures)</u>

Pile Dia. in mm	Pile Depth* in m	Axial (Comp.) Capacity in T	Axial (Uplift) Capacity in T	Lateral Capacity in T (Fix Head)	Depth of Fixity in m
400	14	36	36	2.6	4
450	14	42	41	3.3	5
500	14	47	46	4.1	5
600	14	58	57	5.9	6

From cut-off level.

Note:

a. Cut-off level considered at 1.0 m below EGL.

Summary of Pile Capacity Table For Bored Cast-In Situ Pile – (For Solar Panel)

Pile Dia. in mm	Pile Depth* in m	Axial (Comp.) Capacity in T	Axial (Uplift) Capacity in T	Lateral Capacity in T (Free Head) – 5 mm deflection	Depth of Fixity in m
	1.5	3	2	0.6	3.0
300	2.0	3	3	0.6	3.0
	3.0	6	5	0.6	3.0

From cut-off level.

Note:

- a. Cut-off level considered at 1.0 m below EGL.
- b. Top 3 m soil has high swelling potential. Designer should check for this aspect.
 Pile capacities provided as per client's requirement.

RESULT TABLE - SUBGRADE SOIL SAMPLE

		Res	sult	
Sr. No	Test	S. No. 212209955 *Vastan Mines	S. No. 212209956 *Vastan South Mines	Test Method
	Grain Size Analysis			
	Gravel %	04	09	
1	Coarse Sand %	06	07	IS 2720 (Part-4)
T	Medium Sand %	23	14	2015
	Fine Sand %	23	25	
	Silt + Clay %	44	45	
	Atterberg's Limit			
2	Liquid Limit in %	73	55	IS 2720 (Part-5)
2	Plastic Limit in %	30	29	2015
	Plasticity Index in %	43	26	
3	I.S. Classification	SC	SC	-
4	Modified Proctor Test Maximum Dry Density in gms/cc Optimum Moisture Content in %	1.64 19.00	1.93 17.00	IS 2720 (Part-8) 2015
5	CBR (Soak) Value in %	1.9	2.5	IS 2720 (Part-16) 2016
6	Free Swell Index in %	67	56	IS 2720 (Part-40) 2016

RESULT TABLE – TRIAL PIT – VASTAN SITE

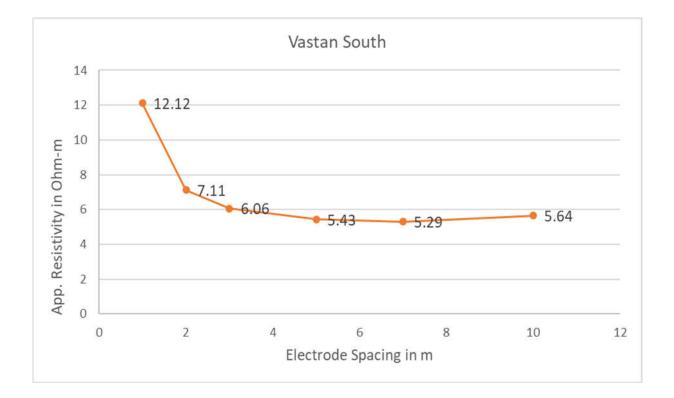
			Result		
Sr. No.	Test	S. No. 212209957 *(Trial Pit- 1m)	S. No. 212209958 *(Trial Pit- 2m)	S. No. 212209959 *(Trial Pit- 3m)	Test Method
1	Moisture Content in %	22.72	33.46	31.32	IS 2720 (Part-2) 2015
	Grain Size Analysis				
	Gravel %	04	00	04	
2	Coarse Sand %	04	05	06	IS 2720 (Part-4)
2	Medium Sand %	05	07	05	2015
	Fine Sand %	10	18	11	
	Silt + Clay %	81	70	74	
	Atterberg's Limit				
3	Liquid Limit in %	47	79	61	IS 2720 (Part-5)
5	Plastic Limit in %	23	34	29	2015
	Plasticity Index in %	24	45	32	
4	I.S. Classification	CI	СН	СН	-
5	Free Swell Index in %	50	75	64	IS 2720 (Part-40) 2016

			Result		
Sr.	Test	S. No.	S. No.	S. No.	Test Method
No.		212209960	212209961	212209962	
		*(Trial Pit- 1m)	*(Trial Pit- 2m)	*(Trial Pit- 3m)	
1	Moisture Content	14.99	12.26	10.09	IS 2720 (Part-2)
	in %	14.99	12.36	19.98	2015
	Grain Size Analysis				
	Gravel %	21	30	11	
2	Coarse Sand %	12	10	11	IS 2720 (Part-4)
2	Medium Sand %	18	11	20	2015
	Fine Sand %	20	17	17	
	Silt + Clay %	29	32	41	
	Atterburg's Limit				
	Liquid Limit in %	48	45	59	IS 2720 (Part-5)
3	Plastic Limit in %	24	24	30	2015
	Plasticity Index in				2015
	%	24	21	29	
4	I.S. Classification	SC	SC	SC	-
5	Free Swell Index in	27	27	55	IS 2720 (Part-
J	%	۷.	۷.		40) 2016

ELECTRICAL RESISTIVITY TEST RESULTS

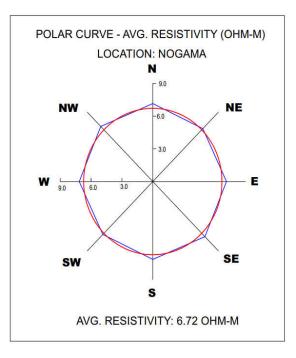
Test			N-S	N	JW-SE		E-W	S	SW-NE
Location	Electrode Spacing in m.	R in Ohm	Apparent Resistivity in ohm-m						
	1.0	1.88	11.8	1.79	11.2	1.88	11.8	2.17	13.6
Vastan	2.0	0.55	7.0	0.59	7.4	0.58	7.3	0.54	6.8
South, N- 21°23'20.0",	3.0	0.32	6.0	0.35	6.6	0.32	6.0	0.30	5.6
E-	5.0	0.16	5.0	0.18	5.6	0.18	5.6	0.18	5.5
73°04'51.0"	7.0	0.13	5.6	0.12	5.4	0.11	4.7	0.12	5.5
	10.0	0.10	6.0	0.08	4.9	0.09	5.8	0.09	5.9

ERT-1 (Vastan South)



Project No.: 2122222

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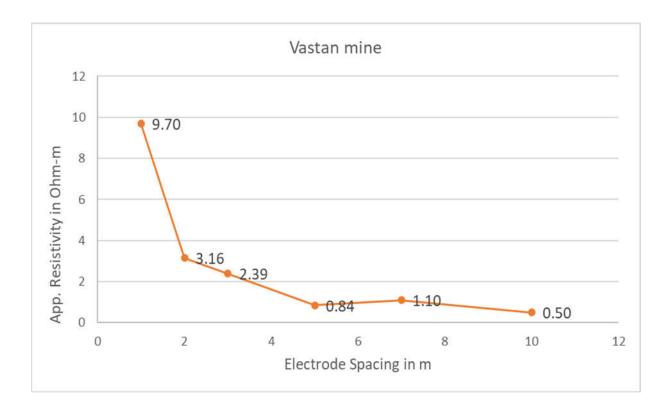


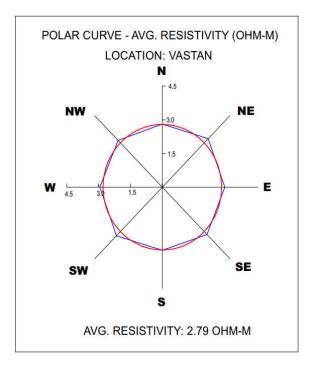
ERT-2 (Vastan)

Test			N-S	N	W-SE		E-W	S	W-NE
Location	Electrode Spacing in m.	R in Ohm	Apparent Resistivity in ohm-m						
	1.0	1.48	9.3	1.51	9.5	1.57	9.9	1.61	10.1
Vastan	2.0	0.23	2.9	0.26	3.3	0.25	3.1	0.26	3.3
mine, N- 21°25'45.7",	3.0	0.12	2.3	0.13	2.5	0.12	2.3	0.13	2.5
E-	5.0	0.03	0.8	0.03	0.9	0.03	0.8	0.03	0.8
73°06'47.5"	7.0	0.02	1.1	0.03	1.1	0.02	1.1	0.03	1.1
	10.0	0.01	0.5	0.01	0.5	0.01	0.5	0.01	0.5

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I. S. CLASSIFICATION

GW: Well graded gravels, gravel-sand mixture or no fines.

- GP: Poorly graded gravels or gravel sand mixture, little or no fines.
- GM: Silty gravels, poorly graded gravel-sand-silt mixtures.
- GC: Clayey gravels, poorly graded gravel-sand-clay mixtures.
- SW: Well-graded sands, gravely sands; little or no fines.
- SP: Poorly graded sands or gravely sands, little or no fines.
- SM: Silty sands, poorly graded sand-silt mixtures.
- SC: Clayey sands, poorly graded sand-clay mixtures.
- ML: Inorganic silt and very fine sands rock flour; silty or clayey fine sands or clayey silts with non-to low plasticity.
- CL: Inorganic clays, gravely clays, sandy clays, silty clays, lean clays of low plasticity.
- OL: organic silts and organic silty clay of low plasticity.
- MI: Inorganic silts, silty or clayey fine sands or clayey silts of medium plasticity.
- CI: Inorganic clays, gravely clays, sandy clays, silty clays, lean clays of medium plasticity.
- OI: Organic silts and organic silty clays of medium plasticity.
- **MH**: Inorganic silt of highly compressibility, micaceous or diatomaceous fine sandy or silty soils, elastic silts.
- CH: Inorganic clays of high plasticity, fat clays.
- OH: Organic Clays of medium to high plasticity.
- Pt: Peat and other highly organic soil with very high compressibility.

TABLE - 3

RESULTS OF STANDARD PENETRATION TEST

Project No. 2122222

Bore Hole No. 1

RL		Blows for Pene		Ns (Blows	Nc(Corrected	N. M. C.
in mts.	0 - 150 mm	150 - 300 mm	300 - 450 mm	/300 mm)	value of Ns)	(in %)
44.23	03	04	06	10	10	24.78
43.23						25.90
42.23	03	07	08	15	15	26.01
41.23						26.54
40.23	05	08	10	18	18	24.93
39.23						27.10
37.73	07	09	14	23	23	28.67
36.23						29.64
35.23	08	11	17	28	28	28.30

TABLE - 5PARTICLE SIZE ANALYSIS

Project No. : 2122222

Bore Hole No. : 1

Soil Strata	RL	Gravel in %		Sand in %		Silt iٍn %
	Sample Type	(>4.75 mm)	(4.75 - 2 mm)	(2mm - 425µ)	(425 - 75 µ)	Clay in %
45.23 to 43.23	44.23/S	4	29	30	6	31
43.23 to 41.23	43.23/U —	4	17	8	13	30 + 28
43.23 to 41.23	42.23/S	0	12	18	18	52
41.23 to 39.23	41.23/U —	20	20	10	15	22 + 13
41.23 to 39.23	40.23/S	3	17	20	20	40
39.23 to 34.73	39.23/U — 	1	5	2	8	36 + 48
39.23 to 34.73	37.73/S	0	4	5	12	79
39.23 to 34.73	36.23/U —	2	10	9	11	32 + 36
39.23 to 34.73	35.23/S — 	0	5	9	4	82

TABLE - 7AUNCONFINED COMPRESSION TEST TABLE

Project No. : 2122222

Bore Hole No. : 1

RL Sample (mts.)	Type of Sample (UD/Rm)	Qu (Kg/cm²)	Cu (Kg/cm²)
41.23 -	UD(Undisturbed)	1.76	
39.23 -	UD(Undisturbed)	2.34	
36.23 -	UD(Undisturbed)	3.17	

TABLE - 7BTRIAXIAL SHEAR TEST

Bore Hole No. :

1

Project No. : 2122222

RL	Sample Type	Normal Stress	Cell Pressure	Pore Pressure	Shear Value	s from Graph
Sample	(UD/Rm)	at Failure	(Kg/cm²)	(Kg/cm²)	Cuu (Kg/cm²)	Øuu (Kg/cm²)
43.23	Undisturbed	2.67	0.50	0.00	0.75	11.64
	Undisturbed	3.27	1.00	0.00		
	Undisturbed	4.93	2.00	0.00		



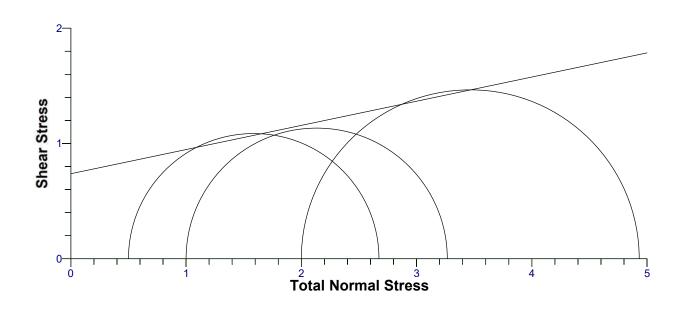
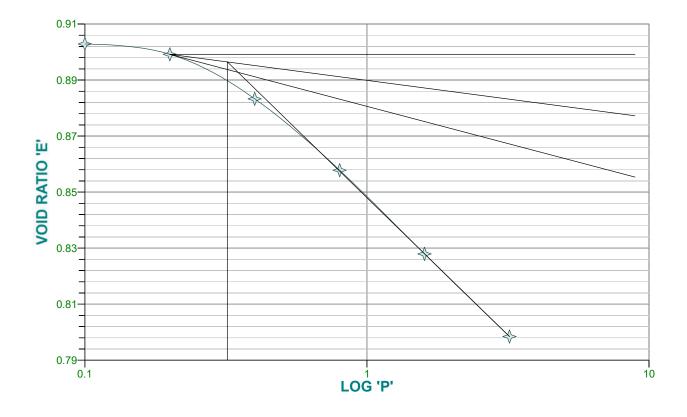


TABLE - 8CONSOLIDATION TEST

Project No.	: 2122222						ole No. :	1
RL	: 41.23 mt		Specific G	ravity : 2.93		Final Mois	ture Cor	itent 28.16 %
Pressure in	Final Readings	Change of of Height	Sample	Change in Ht. in mm	Void Ratio	Coeff. of Vol. Change	T90 in mins	Coeff. of Consolidation
in Kg/cm ²	i teauings	in mm	in mm		Tallo	Mv (cm²/Kg)		Cv (cm²/sec)
0.10	10.769	-0.0390	20.0000	-0.0037	0.9029	1.9500e-02		
0.20	10.730	-0.1670	19.9610	-0.0159	0.8992	4.1832e-02		
0.40	10.563	-0.2680	19.7940	-0.0255	0.8833	3.3849e-02		
0.80	10.295	-0.3140	19.5260	-0.0299	0.8578	2.0101e-02		
1.60	9.981	-0.3100	19.2120	-0.0295	0.8280	1.0085e-02		
3.20	9.671	0.2120	18.9020	0.0202	0.7985	4.6732e-03		
0.80	9.883	0.0680	19.1140	0.0065	0.8186	5.0823e-03		
0.10	9.951		19.1820		0.8251			

Pre-Consolidation Pressure in kg/cm²: 0.33

Cc: 0.09



SUMMARY OF GEOTECHNICAL EXPLORATIONS

Project No. :2122222 Bore Hole No. :1 Project : GIPCL

Bore Hole Started on 23-01-22 Completed on : 23-01-22

Depth of Water Table : Below Termination Level

Method of Drilling :ROTARY DRILLING

Diameter of Bore Hole : 150 mm R. L. of Ground Level :45.23 mt

Location of Bore Hole :N-2365935.75, E-300710.89

RL	I. S.			l Test nples	Ns No. of	Ro	ock	Natural	Der (in gn	sity	Spe-		rticle Analy	e Size	At	terbe _imits	erg	Shri-	Free	ASTAN Shear	Prope		Additional
in metres	Classi- fication	Visual Soil Description	SPT VST	UDS	Blows per 300 mm	C.R. %	RQD	Content	Bulk	Dry	Gra-	Gr. %	Sn %	Silt+ Clay	LL %	PL %	PI %	Lim.	swell Indx %	Test Type	(Kg/ cm²)	Ø in Deg.	Tests or Remarks
45.23	1////	BLACK STIFF PLASTIC CLAYEY SAND		DS																	,		
44.23	sc		SPT	DS	10			24.78				4	65	31	60	29	31		64				
43.23		REDDISH STIFF HIGH PLASTIC CLAY WITH SAND		UDS				25.90	1.85	1.47	2.97	4	38	30+28	67	33	34		50	Tuu	0.75	11.6°	
42.23	CH		SPT	DS	15			26.01				0	48	52	62	24	38		58				
41.23		REDDISH VERY STIFF PLASTIC CLAYEY SAND WITH GRAVEL		UDS				26.54	1.89	1.50	2.93	20	45	22+13	49	23	26			UCC			
40.23	sc		SPT	DS	18			24.93				3	57	40	39	23	16						
39.23		REDDISH VERY STIFF HIGH PLATIC CLAY WITH SAND		UDS				27.10	1.91	1.51	2.84	1	15	36+48	83	33	50			UCC			
37.73	СН		SPT	DS	23			28.67				0	21	79	76	33	43						
36.23				UDS				29.64	1.97	1.52	3.14	2	30	32+36	59	30	29			UCC			
35.23 34.73		TERMINATION	SPT	DS	28			28.30				0	18	82	55	28	27						
SPT -		Penetration Test DS - Disturbed Samp bed Sample VST - Vane Shear Tes	le t	Gr - G Sn - S	iravel Sand	LL - PL -	Liquie	d Limit ic Limit	P C	I - Pla	asticity Shear I	Inde: Parar	x neter	rs N					dation Chan		R Co 2D - R	ore Red ock Qu	covery Jality Designation
																P\/				3			<u> </u>

UNIQUE ENGINEERING TESTING AND ADVISORY SERVICES

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TABLE - 3

RESULTS OF STANDARD PENETRATION TEST

Project No. 2122222

Bore Hole No. 2

RL	No. of	Blows for Penet		Ns (Blows	Nc(Corrected	N. М. С.
in mts.	0 - 150 mm	150 - 300 mm	300 - 450 mm	/300 mm)	value of Ns)	(in %)
48.02	02	07	09	16	25	19.98
47.02						18.63
46.02	06	09	14	23	23	19.38
45.02						19.18
44.02	06	09	16	25	25	22.47
43.02						23.86
41.52	10	13	20	33	33	27.00
40.02						26.29
39.02	14	19	25	44	44	26.67

TABLE - 5PARTICLE SIZE ANALYSIS

Project No. : 2122222

Bore Hole No. : 2

Coll Cturate	RL	Gravel in %		Sand in %		Silt iٍn %
Soil Strata	Sample Type	(>4.75 mm)	(4.75 - 2 mm)	(2mm - 425µ)	(425 - 75 µ)	Clay in %
49.016 to 48.016	49.02/D	19	20	15	7	39
48.016 to 47.016	48.02/S —	27	35	26	3	9
47.016 to 41.516	47.02/U — 	8	35	17	5	22 + 13
47.016 to 41.516	46.02/S	7	30	23	6	34
47.016 to 41.516	45.02/U – - -	5	26	19	10	18 + 22
47.016 to 41.516	44.02/S — 	8	23	25	8	36
47.016 to 41.516	43.02/U — 	8	22	18	10	17 + 25
41.516 to 38.516	41.52/S _ _ _ _ _ _ _	1	11	14	14	60
41.516 to 38.516	40.02/U — 	2	9	10	10	31 + 38
41.516 to 38.516	39.02/S — 	1	15	17	16	51

TABLE - 7A

UNCONFINED COMPRESSION TEST TABLE

Project No. : 2122222

Bore Hole No. : 2

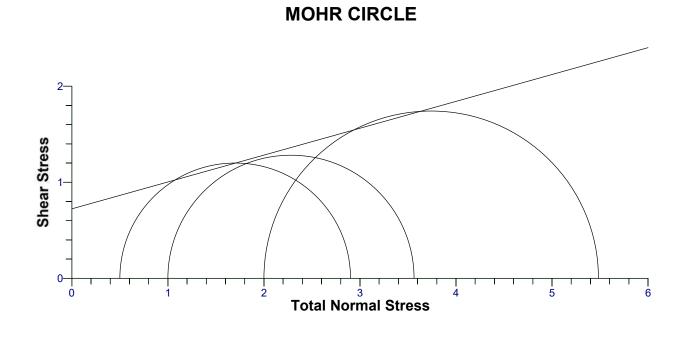
RL Sample (mts.)	Type of Sample (UD/Rm)	Qu (Kg/cm²)	Cu (Kg/cm²)
47.02	UD(Undisturbed)	0.92	
43.02	UD(Undisturbed)	2.18	
40.02	UD(Undisturbed)	2.83	

TABLE - 7BTRIAXIAL SHEAR TEST

Project No. : 2122222

Bore Hole No.: 2

RL	Sample Type	Normal Stress	Cell Pressure	Pore Pressure	Shear Value	s from Graph
Sample	(UD/Rm)	at Failure	(Kg/cm²)	(Kg/cm²)	Cuu (Kg/cm²)	Øuu (Kg/cm²)
45.02	Undisturbed	2.90	0.50	0.00	0.73	15.95
	Undisturbed	3.56	1.00	0.00		
	Undisturbed	5.48	2.00	0.00		



SUMMARY OF GEOTECHNICAL EXPLORATIONS

Project No. :2122222 Bore Hole No. :2 Project : GIPCL

Bore Hole Started on 21-01-22 Completed on : 21-01-22

Depth of Water Table : Below Termination Level

Method of Drilling :ROTARY DRILLING

Diameter of Bore Hole : 150 mm R. L. of Ground Level :49.02 mt

Location of Bore Hole :N-2366409.57, E-300954.22

RL	I. S.		Field		Ns	Rock	Natura	Den	sity	Spe-	Pa	rticle	Size	At	terbe	erg	Shri-	Free		Prope		Additional
	Classi-	Visual Soil Description	/San SPT	UDS	No. of Blows per 300 mm	C.R. RC	Moist.	(in gr	ns/cc) Dry	Gra- vity	Gr.	Analy Sn	/sis Silt+		Limits PL %	s PI %	nkge Lim. %	swell Indx %	Test Type	C (Kg/ cm²)	_Ø _in	Tests or Remarks
49.02		REDDISH YELLOW PLASTIC CLAYEY	VST	DS DS	300 mm	% %	> %	Duik	Diy	vity	% 19		Clay 39			% 13	%	% 30	турс	cm ²)	Deg.	
	sc	SAND WITH GRAVEL		50									00									
48.02	· · · · · · · · · · · · · · · · · · ·	BROWNISH SILT WITH MEDIUM TO COARSE SAND AND GRAVEL	SPT	DS	16		19.98				27	64	9		-	-						
47.02		YELLOW VERY STIFF PLASTIC CLAYEY SAND		UDS			18.63	1.85	1.56	2.77	8	57	22+13	51	27	24		55	UCC			
46.02			SPT	DS	23		19.38				7	59	34	55	28	27		41				
45.02				UDS			19.18	1.91	1.60	2.78	5	55	18+22	63	31	32			Tuu	0.73	16.0°	
44.02	SC		SPT	DS	25		22.47				8	56	36	63	31	32						
43.02				UDS			23.86	1.98	1.60	2.80	8	50	17+25	62	30	32			UCC			
41.52	// // // ٨	REDDISH HARD HIGH PLASTIC CLAY WITH SAND	SPT	DS	33		27.00				1	39	60	53	26	27						
40.02	Сн			UDS			26.29	1.97	1.56	2.99	2	29	31+38	58	29	29			UCC			
39.02 38.52			SPT	DS	44		26.67				1	48	51	52	26	26						
SPT - S	Standard	TERMINATION Penetration Test DS - Disturbed Sample VST - Vane Shear Test	e	Gr - G	iravel	LL - Liq	uid Limit astic Limit	P P	I - Pla	asticity Shear I	Inde	×.	(onsoli		<u> </u>	R Co	ore Rec	covery ality Designation
UDS - I	Jndisturb	ed Sample VST - Vane Shear Test		Šn - Š											Coeff. RV			Chan	ge R(R - ענ	ock Qu	ality Designation

UNIQUE ENGINEERING TESTING AND ADVISORY SERVICES

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TABLE - 3

RESULTS OF STANDARD PENETRATION TEST

Project No. 2122222

Bore Hole No. 3

RL		Blows for Pene		Ns (Blows	Nc(Corrected	N. M. C.
in mts.	0 - 150 mm	150 - 300 mm	300 - 450 mm	/300 mm)	value of Ns)	(in %)
42.17	03	05	07	12	12	19.23
41.17	10	10	13	23	30	13.72
40.17-	30	50/200	-	50/200	59/200	19.92
39.17-						22.69
37.17	07	11	18	29	27	15.68
34.17	38	58/200	-	58/200	58/200	28.24
33.17—	50/150	-	-	50/150	50/150	35.88
_						

Project No. : 2122222

Soil Strata	RL	Gravel in %		Sand in % Silt in % (4.75 - 2 mm) (2mm - 425μ) (425 - 75 μ) Clay in %									
Soli Strata	Sample Type	(>4.75 mm)	(4.75 - 2 mm)	(2mm - 425µ)	(425 - 75 µ)	Clay in %							
43.165 to 41.165	43.17/D — _ _	2	6	4	9	79							
43.165 to 41.165	42.17/S –	0	10	9	10	71							
41.165 to 40.165	41.17/S —	63	13	8	7	9							
40.165 to 34.165	40.17/S	5	58	19	2	16							
40.165 to 34.165	39.17/D — 	2	31	46	6	15							
40.165 to 34.165	 37.17/S 	5	22	23	26	24							
34.165 to 32.665	 34.17/S	5	8	8	12	67							
34.165 to 32.665	33.17/S — 	0	4	1	11	84							

Project No. :2122222 Bore Hole No. :3 Project : GIPCL

Bore Hole Started on :19-01-22 Completed on : 20-01-22

Depth of Water Table : Below Termination Level

Method of Drilling :SHELL & AUGER

Diameter of Bore Hole : 150 mm R. L. of Ground Level :43.17 mt

Location of Bore Hole :N-2366995.48, E-301486.95

RL	I. S.			Test	Ns	Ro	cķ	Natural	Den	sity	Spe-	Pa		Size	At	terbe	erg	Shri-	Free	ASTAN Shear	Prope	rties	Additional
in	Classi- fication	Visual Soil Description	/San SPT	nples UDS	No. of Blows per 300 mm	C.R.		Moist. Content	(in gm Bulk	ns/cc) Drv	cific Gra- vity	Gr.	Analy Sn	Silt+	LL %	_imits	s Pl	nkge Lim.	swell Indx %	Test Type	C (Kg/ cm²)	Ø in	Tests or Remarks
43.17	///////////////////////////////////////	BLACK STIFF HIGH PLASTIC CLAY WITH SAND	V51	DS	300 mm	%	70	%			vity	2	% 19	Clay 79			% 24	%	% 43	51	cm ²)	Deg.	
42.17	СН		SPT	DS	12			19.23				0	29	71	64	28	36		50				
41.17		YELLOW SANDY GRAVEL (HIGHLY WEATHERED ROCK)	SPT	DS	23			13.72				63	28	9		-	-						
40.17		YELLOW DENSE SILTY MEDIUM TO COARSE SAND WITH BOULDERS	SPT	DS	50/200			19.92				5	79	16	24	-	-						
39.17				DS				22.69				2	83	15	23	-	-						
38.17				DS																			
37.17	SM		SPT	DS	29			15.68				5	71	24	27	-	-						
35.67				DS																			
34.17	//////	YELLOW CEMENTED HIGH PLASTIC CLAY WITH SAND	SPT	DS	58/200			28.24				5	28	67	71	31	40						
33.17	<u>CH</u>		SPT	DS	50/150			35.88				0	16	84	74	32	42						
		TERMINATION Penetration Test DS - Disturbed Samp bed Sample VST - Vane Shear Tes		Gr - C Sn - S				d Limit ic Limit			sticity hear F			s N	/v - (Coeff.	of Vo	olume	dation Chan	C. ge R	 .R C(QD - R	ore Rec ock Qu	covery ality Designation
	UNIQUE ENGINEERING TESTING AND ADVISORY SERVICES																						

UNIQUE ENGINEERING TESTING AND ADVISORY SERVICES

TABLE - 3

RESULTS OF STANDARD PENETRATION TEST

Project No. 2122222

RL		Blows for Pene		Ns (Blows	Nc(Corrected	N. M. C.
in mts.	0 - 150 mm	150 - 300 mm	300 - 450 mm	/300 mm)	value of Ns)	(in %)
53.81	02	04	09	13	13	26.45
52.81						23.10
51.81	03	05	07	12	12	24.30
50.81						24.51
49.81	05	06	09	15	15	25.25
48.81						26.82
47.31	03	04	06	10	10	24.57
45.81						28.87
44.31	04	06	08	14	14	29.78
42.81	05	08	09	17	17	27.62
41.31						26.74
39.81	07	09	11	20	20	27.15

Project No. : 2122222

Dire Tojeet No 2 122222											
Soil Strata	RL Sampla Type	Gravel in %	(1.75 2 mm)	Sand in %	(125 75)	Silt in %					
	Sample Type	(>4.75 mm)	(4.75 - 2 mm)	(2mm - 425µ)	(425 - 75 µ)	Clay in %					
54.81 to 51.81	54.81/D —	1	5	13	10	71					
54.81 to 51.81	53.81/S	3	4	14	15	64					
54.81 to 51.81	52.81/U	0	6	5	12	34 + 43					
51.81 to 48.81	51.81/S	0	5	2	15	78					
51.81 to 48.81	50.81/U	0	5	3	15	37 + 40					
51.81 to 48.81	49.81/S	0	0	8	13	79					
48.81 to 42.81	48.81/U	0	6	8	16	26 + 44					
48.81 to 42.81	47.31/S	0	10	11	5	74					
48.81 to 42.81	45.81/U	0	4	3	9	23 + 61					
48.81 to 42.81	44.31/S	0	5	6	9	80					
42.81 to 39.31	42.81/S	0	4	30	11	55					
42.81 to 39.31	41.31/U	0	6	4	7	26 + 57					
42.81 to 39.31	39.81/S	0	5	8	5	82					

TABLE - 7A

UNCONFINED COMPRESSION TEST TABLE

Project No. : 2122222

RL Sample (mts.)	Type of Sample (UD/Rm)	Qu (Kg/cm²)	Cu (Kg/cm²)
52.81	UD(Undisturbed)	0.99	
48.81	UD(Undisturbed)	1.23	
45.81	UD(Undisturbed)	0.94	
41.31	UD(Undisturbed)	1.65	

TABLE - 7BTRIAXIAL SHEAR TEST

Project No. : 2122222

Bore Hole No. :	
re Pore Pressure Shear Values from Gra	aph

RL	Sample Type	Normal Stress	Cell Pressure Pore Pressure		Normal Stress Cell Pressure Pore Pressure Shear				
Sample	(UD/Rm)	at Failure	(Kg/cm²)	(Kg/cm²)	Cuu (Kg/cm ²)	Øuu (Kg/cm²)			
50.81	Undisturbed	2.47	0.50	0.00	0.73	11.34			
	Undisturbed	3.33	1.00	0.00					
	Undisturbed	4.71	2.00	0.00					



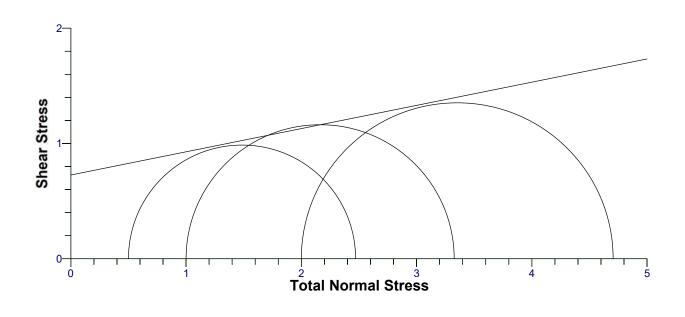
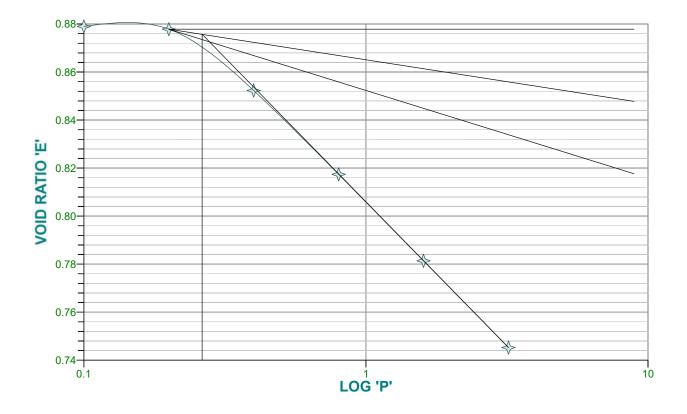


TABLE - 8CONSOLIDATION TEST

Project No.	: 2122222			Bore H	ole No. :	4		
RL	: 50.81 mt		Specific G	ravity : 2.93		Final Mois	ture Con	tent 26.72 %
Pressure in in Kg/cm²	Final Readings	Change of of Height in mm	Height of Sample in mm	Change in Ht. in mm	Void Ratio	Coeff. of Vol. Change Mv (cm²/Kg)	T90 in mins	Coeff. of Consolidation Cv (cm²/sec)
0.10	9.851	0.0400	20.0000	0.0011	0.8790	6.0000e-03		
0.20	9.839	-0.0120 -0.2720	19.9880	-0.0011 -0.0256	0.8779	6.8041e-02		
0.40	9.567	-0.3720	19.7160	-0.0230	0.8523	4.7170e-02		
0.80	9.195	-0.3830	19.3440	-0.0360	0.8174	2.4749e-02		
1.60	8.812	-0.3850	18.9610	-0.0362	0.7814	1.2691e-02		
3.20	8.427	0.2670	18.5760	0.0251	0.7452	5.9889e-03		
0.80	8.694	0.1450	18.8430	0.0136	0.7703	1.0993e-02		
0.10	8.839	0.1400	18.9880	0.0100	0.7839	1.00000 02		

Pre-Consolidation Pressure in kg/cm²: 0.26

Cc: 0.12



Project No. :2122222

Bore Hole No.

Project : GIPCL

Bore Hole Started on 24-01-22 Completed on : 25-01-22

Depth of Water Table : Below Termination Level

Method of Drilling :ROTARY DRILLING

:4

Diameter of Bore Hole : 150 mm R. L. of Ground Level : 54.81 mt

Location of Bore Hole :N-2370585.72, E-304656.24

RL	I. S.			l Test	Ns	Ro	ck	Natural	, Den	sity	Spe-	Pa	rticle	Size	At	terbe	rg	Shri-	Free	ASTAN Shear			Additional
in	Classi- fication	Visual Soil Description			No. of Blows per 300 mm	C.R.	RQD	Moist. Content	(in gr	Dry	Gra- vity	Gr.	Analy Sn	/sis Silt+	LL	_imits PL %	PI	nкge Lim. %	swell Indx %	Test Type	C (Kg/ cm²)	Ø in	Tests or Remarks
			VST		300 mm	%	%	%	Duik	Diy	vity	%					% 37	%		турс	cm²)	Deg.	Terriarks
54.81		YELLOWSTIFF HIGH PLASTIC CLAY WITH SAND(FILLING)		DS								1	28	71	70	33	31		50				
53.81			SPT	DS	13			26.45				3	33	64	56	28	28		38				
52.81	CH			UDS				23.10	1.79	1.46	2.84	0	23	34+43	69	33	36		56	UCC			
51.81		BLACK STIFF HIGH PLASTIC CLAY	SPT	DS	12			24.30				0	22	78	63	31	32						
50.81	СН	WITH SAND		UDS				24.51	1.84	1.48	2.93	0	23	37+40	59	30	29			Tuu	0.73	11.3°	
49.81			SPT	DS	15			25.25				0	21	79	63	30	33						
48.81		REDDISH STIFF HIGH PLASTIC CLAY WITH SAND		UDS				26.82	1.89	1.49	2.84	0	30	26+44	72	33	39			UCC			
47.31			SPT	DS	10			24.57				0	26	74	82	36	46						
45.81	СН			UDS				28.87	1.84	1.43	2.87	0	16	23+61	86	37	49			UCC			
44.31			SPT	DS	14			29.78				0	20	80	85	35	50						
42.81		BLACK STIFF HIGH PLASTIC CLAY	SPT	DS	17			27.62				0	45	55	68	31	37						
41.31	СН			UDS				26.74	1.91	1.50	2.88	0	17	26+57	77	34	43			UCC			
39.81 39.31		TERMINATION	SPT	DS	20			27.15				0	18	82	65	31	34						
SPT -	Standard	Penetration Test DS - Disturbed Samp	e	Gr - G Sn - S	iravel	LL -	Liquio	d Limit ic Limit	P	I-Pla	asticity	Inde	X Neter	(Coeff.	of Co	onsolio	dation	C.	R C	ore Rec	overy
003-	SPT - Standard Penetration Test DS - Disturbed Sample Gr - Gravel LL - Liquid Limit PI - Plasticity Index Cv - Coeff. of Consolidation C.R Core Recovery JDS - Undisturbed Sample VST - Vane Shear Test Sn - Sand PL - Plastic Limit PI - Plastic Plastic Limit Mv - Coeff. of Volume Change CR - Core Recovery JDS - Undisturbed Sample VST - Vane Shear Test Sn - Sand PL - Plastic Limit PI - Shear Parameters Mv - Coeff. of Volume Change RQD - Rock Quality Designation																						

UNIQUE ENGINEERING TESTING AND ADVISORY SERVICES

TABLE - 3

RESULTS OF STANDARD PENETRATION TEST

Project No. 2122222

RL		Blows for Penet		Ns (Blows	Nc(Corrected	N. M. C.
in mts.	0 - 150 mm	150 - 300 mm	300 - 450 mm	/300 mm)	value of Ns)	(in %)
48.85	03	03	04	07	07	24.62
47.85						23.90
46.85	03	06	05	11	11	23.93
45.85						24.12
44.85	06	09	11	20	20	25.68
43.85						25.89
42.35	07	10	13	23	23	25.29
40.85						25.65
39.35	06	09	12	21	21	25.19
37.85						26.16
36.35	07	11	15	26	26	26.78
34.85	06	10	17	27	27	26.84

Project No. : 2122222

RL Gravel in % Sand in %										
Soil Strata	Sample Type	(>4.75 mm)	(4 75 - 2 mm)	(2mm - 425µ)	(425 - 75 µ)	Silt in % Clay in %				
49.85 to 47.85	49.85/D	0	4	12	12	72				
49.85 to 47.85	48.85/S —	0	6	6	4	84				
47.85 to 44.85	47.85/U 🗌	0	0	5	7	41 + 47				
47.85 to 44.85	46.85/S	0	6	6	5	83				
		-		_	_					
47.85 to 44.85	45.85/U	1	5	6	5	41 + 42				
+1.00 10 ++.00		I		0	5	71 72				
44.05 to 07.05		4	7	4	0	00				
44.85 to 37.85	44.85/S	1	7	1	9	82				
44.85 to 37.85	43.85/U	4	8	4	4	39 + 41				
44.85 to 37.85	42.35/S =	0	6	6	9	79				
44.85 to 37.85	40.85/U	3	4	3	7	44 + 39				
		-			-					
11 95 to 27 95	39.35/S	0	5	5	6	04				
44.85 to 37.85	39.35/5 -	0	5	5	0	84				
37.85 to 34.35	37.85/U	0	6	2	6	30 + 56				
37.85 to 34.35	36.35/S =	0	6	5	6	83				
37.85 to 34.35	34.85/S	0	6	2	3	89				
	-		Ŭ	_	Č					
L										

TABLE - 7A

UNCONFINED COMPRESSION TEST TABLE

Project No. : 2122222

RL Sample (mts.)	Type of Sample (UD/Rm)	Qu (Kg/cm²)	Cu (Kg/cm²)
47.85	UD(Undisturbed)	1.02	
43.85	UD(Undisturbed)	2.06	
40.85	UD(Undisturbed)	2.38	
37.85	UD(Undisturbed)	3.05	

TABLE - 7BTRIAXIAL SHEAR TEST

Project No. : 2122222

Bore Hole No. :	5

RL		Normal Stress	Cell Pressure	Pore Pressure	Shear Values	s from Graph
Sample	(UD/Rm)	at Failure	(Kg/cm²)	(Kg/cm²)	Cuu (Kg/cm²)	Øuu (Kg/cm²)
45.85	Undisturbed	2.32	0.50	0.00	0.76	6.49
	Undisturbed	2.97	1.00	0.00		
	Undisturbed	4.21	2.00	0.00		



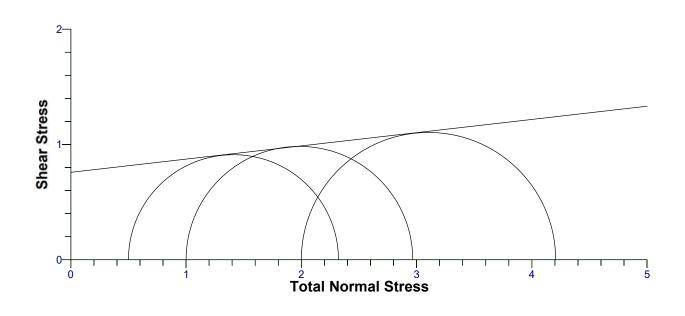
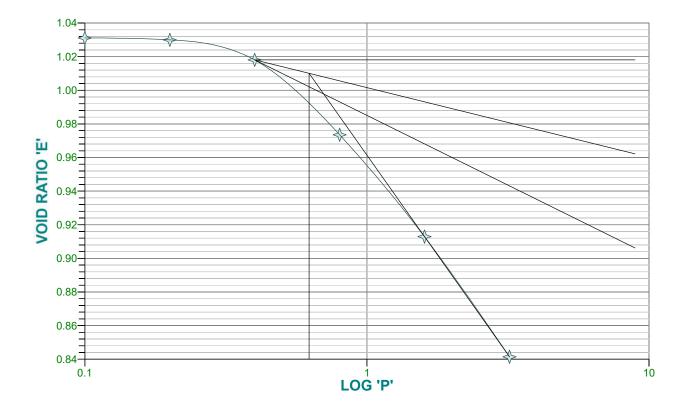


TABLE - 8CONSOLIDATION TEST

Project No.	: 2122222					Bore H	ole No. :	5
RL	: 43.85 mt		Specific Gr	avity : 2.93		Final Mois	ture Con	tent 29.14 %
Pressure in in Kg/cm ²	Final Readings	Change of of Height in mm		Change in Ht. in mm	Void Ratio	Coeff. of Vol. Change Mv (cm²/Kg)	T90 in mins	Coeff. of Consolidation Cv (cm²/sec)
0.10	8.853	0.0110	20.0000	0.0011	1.0312	5.4999e-03		
0.20	8.842	-0.0110 -0.1180	19.9890	-0.0011 -0.0120	1.0300	2.9516e-02		
0.40	8.724	-0.4390	19.8710	-0.0446	1.0181	5.5231e-02		
0.80	8.285	-0.5960	19.4320	-0.0605	0.9735	3.8339e-02		
1.60	7.689	-0.7040	18.8360	-0.0715	0.9129	2.3360e-02	2.06	2.8447e-03
3.20	6.985	0.0950	18.1320	0.0096	0.8415	2.1831e-03		2.01110.00
0.80	7.080	0.0340	18.2270	0.0035	0.8511	2.6648e-03		
0.10	7.114	0.0340	18.2610	0.0000	0.8546	2.00100 00		

Pre-Consolidation Pressure in kg/cm²: 0.62





Project No. :2122222 Bore Hole No. :5 Project : GIPCL

Bore Hole Started on 26-01-22 Completed on 27-01-22

Depth of Water Table : Below Termination Level

Method of Drilling :ROTARY DRILLING

Diameter of Bore Hole : 150 mm R. L. of Ground Level :49.85 mt

Location of Bore Hole :N-2371087.04, E-304576.03

RL	I. S.		Field		Ns	_ Ro	cķ	Natural	Den	sity	Spe-	Pa		Size		terbe	erg	Shri-	Free	ASTAN Shear	Prope		Additional
in	Classi-	Visual Soil Description	/San	nples UDS	No. of	Prope		Moist.	(in gr	ns/cc)	cific	A	Analy	/sis Silt+		Limit	S DI	nkge	swell	Test	C	Ø	Tests or
metres	fication		VST	DS	Blows per 300 mm	%	8	%	Bulk	Dry	Gra- vity	% %	%	Clay	%	PL %	ГI %	Lim. %	Indx %	Туре	(Kg/ cm²)	Deg.	Remarks
49.85		YELLOW FIRM HIGH PLASTIC CLAY WITH SAND (FILLING)		DS								0	28	72	51	26	25		25			-	
48.85			SPT	DS	07			24.62				0	16	84	59	30	29		21				
47.85		REDDISH STIFF HIGH PLASTIC CLAY		UDS				23.90	1.79	1.44	2.91	0	12	41+47	59	29	30		33	UCC			
46.85			SPT	DS	11			23.93				0	17	83	59	28	31		42				
45.85	un			UDS				24.12	1.85	1.49	3.00	1	16	41+42	52	26	26			Tuu	0.76	6.5°	
44.85	// // // ٨	BLACK VERY STIFF HIGH PLASTIC	SPT	DS	20			25.68				1	17	82	60	28	32						
43.85		CLAY WITH SAND		UDS				25.89	1.90	1.51	2.93	4	16	39+41	59	30	29			UCC			
42.35			SPT	DS	23			25.29				0	21	79	65	31	34						
40.85	СН			UDS				25.65	1.92	1.53	3.01	3	14	44+39	56	29	27			UCC			
39.35			SPT	DS	21			25.19				0	16	84	55	27	28						
37.85	// // // //	YELLOWISH STIFF HIGH PLASTIC		UDS				26.16	1.95	1.54	2.94	0	14	30+56	70	32	38			UCC			
36.35	СН		SPT	DS	26			26.78				0	17	83	67	32	35						
34.85 34.35	///////	TERMINATION	SPT	DS	27			26.84				0	11	89	81	34	47						
SPT -	Standard	Penetration Test DS - Disturbed Samp	e	Gr - G	iravel	LL -	Liqui	d Limit ic Limit	P	I - Pla	asticity Shear I	Inde	x,	(_v - c	Coeff.	of Co	onsolio	dation	C.	R Co	ore Red	covery ality Designation
UDS - I	Undisturb	ed Sample VST - Vane Shear Test		Šn - Š												Coeff. D\/			Chan	ge R(D - R	ock Qu	ality Designation

UNIQUE ENGINEERING TESTING AND ADVISORY SERVICES

TABLE - 3

RESULTS OF STANDARD PENETRATION TEST

Project No. 2122222

RL	No. of	Blows for Pene	tration	Ns (Blows	Nc(Corrected	N. M. C.
in mts.	0 - 150 mm	150 - 300 mm	300 - 450 mm	/300 mm)	value of Ns)	(in %)
56.19						24.80
55.19	03	03	04	07	07	24.54
54.19						25.33
53.19	02	05	06	11	11	24.67
52.19						25.09
51.19	03	06	08	14	14	25.17
49.69						24.81
48.19	05	06	09	15	15	25.67
46.69						25.40
45.19	07	08	11	19	19	25.71
43.69						26.02
42.19	06	10	13	23	23	26.95

Project No. : 2122222

			[Bore no	
Soil Strata	RL	Gravel in %	(4.75.0.)	Sand in %	(405 35)	Silt in %
	Sample Type	(>4.75 mm)	(4.75 - 2 mm)	(2mm - 425µ)	(425 - 75 µ)	Clay in %
57.19 to 56.19	57.19/D	3	6	7	6	78
56.19 to 54.19	56.19/U –	0	4	5	7	25 + 59
56.19 to 54.19	55.19/S	0	5	5	5	85
54.19 to 52.19	54.19/U	0	5	6	11	25 + 53
54.19 to 52.19	53.19/S	1	8	5	5	81
52.19 to 41.69	52.19/U	5	5	3	7	30 + 50
52.19 to 41.69	51.19/S	2	5	4	3	86
52.19 to 41.69	49.69/U	10	9	3	8	33 + 37
52.19 to 41.69	48.19/S	0	7	5	7	81
52.19 to 41.69	46.69/U	4	7	5	6	31 + 47
52.19 to 41.69	45.19/S	0	8	2	2	88
52.19 to 41.69	43.69/U	10	8	8	6	28 + 40
52.19 to 41.69	42.19/S	0	10	7	5	78

TABLE - 7A

UNCONFINED COMPRESSION TEST TABLE

Project No. : 2122222

RL Sample (mts.)	Type of Sample (UD/Rm)	Qu (Kg/cm²)	Cu (Kg/cm²)
56.19	UD(Undisturbed)	0.75	
52.19	UD(Undisturbed)	1.32	
49.69	UD(Undisturbed)	1.58	
46.69	UD(Undisturbed)	2.08	
43.69	UD(Undisturbed)	2.75	
-	-		

TABLE - 7BTRIAXIAL SHEAR TEST

Project No. : 2122222

RL	Sample Type	Normal Stress	Cell Pressure	Pore Pressure	Shear Values	s from Graph
Sample	(UD/Rm)	at Failure	(Kg/cm²)	(Kg/cm²)	Cuu (Kg/cm ²)	Øuu (Kg/cm²)
54.19	Undisturbed	2.31	0.50	0.00	0.58	12.86
	Undisturbed	2.96	1.00	0.00		
	Undisturbed	4.63	2.00	0.00		
	Ondistarbed	4.00	2.00	0.00		



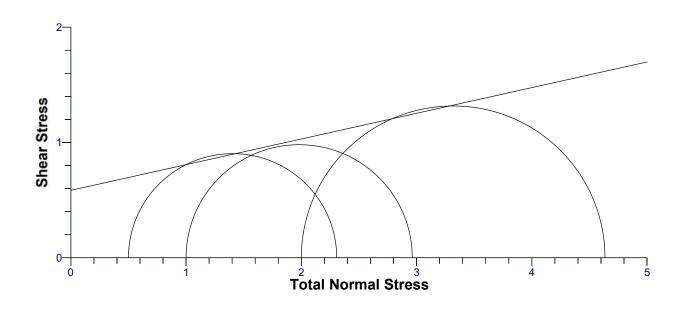
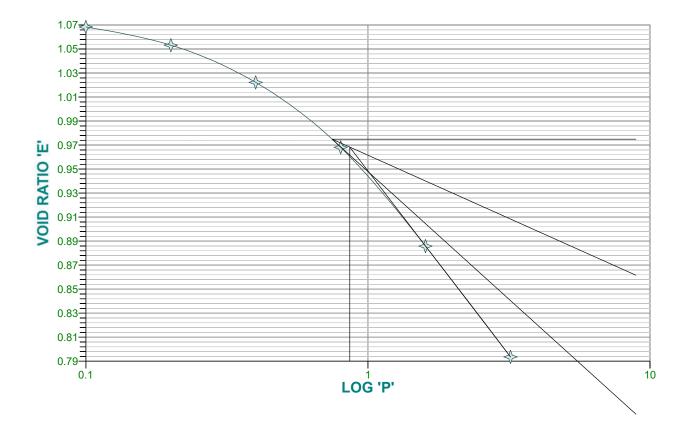


TABLE - 8CONSOLIDATION TEST

Project No.	: 2122222					Bore H	ole No. :	6
RL	: 52.19 mt		Specific G	ravity : 2.91		Final Mois	ture Con	tent 28.55 %
Pressure in in Kg/cm ²	Final Readings	Change of of Height in mm		Change in Ht. in mm	Void Ratio	Coeff. of Vol. Change Mv (cm²/Kg)	T90 in mins	Coeff. of Consolidation Cv (cm²/sec)
0.10	6.711	-0.1470	20.0000	-0.0152	1.0685	7.3500e-02		
0.20	6.564	-0.3000	19.8530	-0.0310	1.0533	7.5555e-02		
0.40	6.264	-0.5230	19.5530	-0.0541	1.0222	6.6870e-02		
0.80	5.741	-0.7950	19.0300	-0.0822	0.9681	5.2220e-02		
1.60	4.946	-0.8930	18.2350	-0.0924	0.8859	3.0607e-02	1.75	3.6508e-03
3.20	4.053	0.0740	17.3420	0.0077	0.7936	1.7780e-03		
0.80	4.127	0.2920	17.4160	0.0302	0.8012	2.3952e-02		
0.10	4.419		17.7080		0.8314			

Pre-Consolidation Pressure in kg/cm²: 0.86

Cc: 0.29



Project No. :2122222

Bore Hole No.

Project : GIPCL

Bore Hole Started on 27-01-22 Completed on : 28-01-22

Depth of Water Table : Below Termination Level

Method of Drilling :ROTARY DRILLING

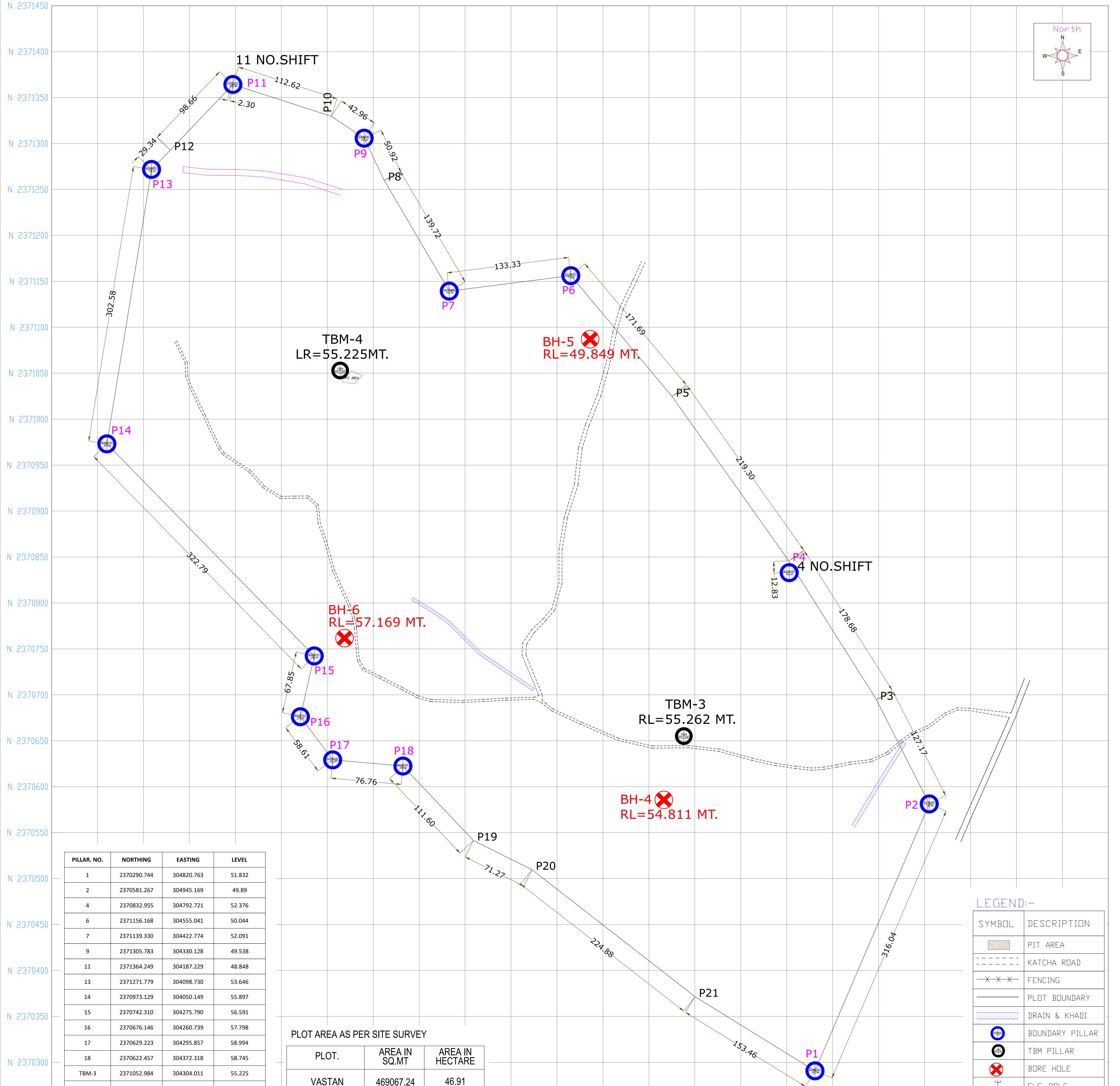
:6

Diameter of Bore Hole : 150 mm R. L. of Ground Level :57.19 mt

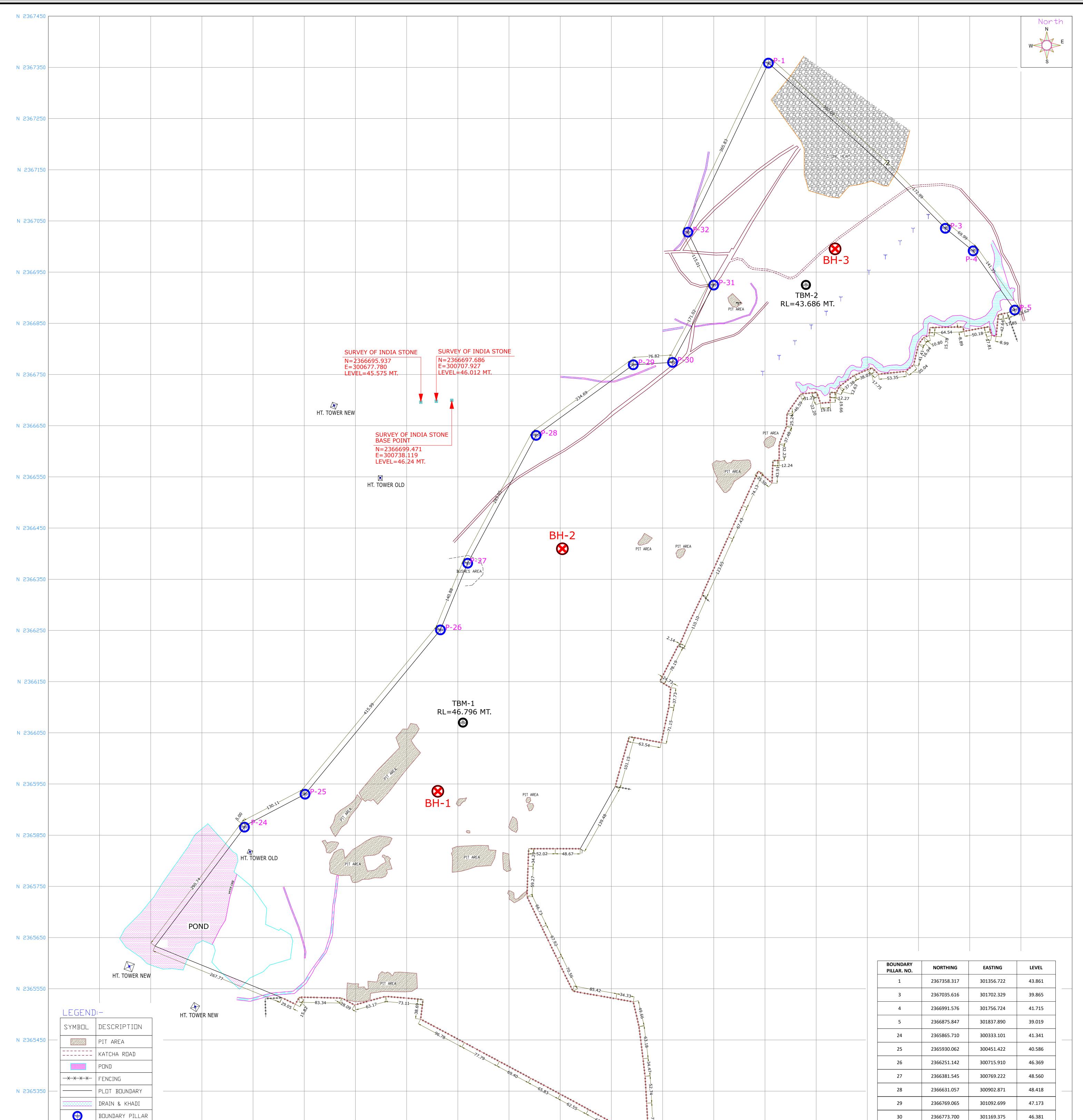
Location of Bore Hole :N-2370761.65, E-304308.73

46.69 CH 45.19 UDS 45.19 DS 19 25.71 1.93 1.54 3.00 4 18 31+47 61 30 31 UCC UCC 43.69 UDS 26.02 1.96 1.55 3.02 10 22 28+40 59 29 30 UCC UCC 42.19 SPT DS 23 26.95 0 22 78 56 28 28 UCC 10	mound	Field Test Ns Rock Natural Density Sper Particle Size Atterberg Shri- Free Spear Properties																						
Inclease- tenters Visual Soil Description Service Service No. of Service Producting Mode (n. Marking Service) L. Inclust (n. Marking Service) I. Inclust (n. Marking Service) Inclust (n. Marking Service) I. Inclust (n. Mar	RI	I. S.				Ns	Ro	ck	Natural	Den	sity	Spe-	Pa	rticle	e Size	At	terbe	erg	Shri-	Free		Prope		Additional
Weither Barling interview Visit Disc 300 mm % % % % % % % % % % % % % % % % % % % % % % % % % % % % % % % % % % % % % % % % % % % % % % % % % % % % % % % % % % % % % % % % % % % % % % % % % % % % % % % % % % % % % % % % % % % % % % % % % % % % % % % % % % % % % % % % % % <td></td> <td></td> <td>Visual Soil Description</td> <td></td> <td>npies</td> <td>No. of</td> <td>Prope</td> <td></td> <td>Moist.</td> <td>(in gr</td> <td>is/cc)</td> <td>cific</td> <td></td> <td>Analy</td> <td>ysis Silt+</td> <td></td> <td></td> <td>S IDI</td> <td>nkge</td> <td>swell</td> <td>Test</td> <td>C</td> <td>Ø</td> <td></td>			Visual Soil Description		npies	No. of	Prope		Moist.	(in gr	is/cc)	cific		Analy	ysis Silt+			S IDI	nkge	swell	Test	C	Ø	
57.19 5H FILLING DS DS P S S S S S S S S S S S S S S S S S S S S S S S S S S S S S S S S S S S S S S S S S S S S S S S S S S S S S S S S S S S S S S S S S S S S S S S S S S S S S S S S S S S S S S S S S S S S S S S S S S S S S S S S S S S S S S S S	metres	fication		VST	DS	300 mm	С.К. %	кор %	%	Bulk	Dry	vity	ЮГ. %	8	Clay	LL %	PL %	8	۲Ш. %	%	Туре	cm^{2}	Deg.	Remarks
SPT DS 07 24.54 0 15 85 69 33 36 100 54.19 MITH SAND SPT DS 07 24.54 25.33 1.86 1.49 2.84 0 22 25+53 67 32 35 67 Tuu 0.58 12.9* 53.19 Of MITH SAND SPT DS 11 24.67 18 81 62 31 31 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00	57.19		FILLING																			,		
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UNIQUE ENGINEERING TESTING AND ADVISORY SERVICES



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					DATE	02.02.2022	1CM.=25.0 MT.		Udhna, Surat-39 Mail ID + <u>uniq</u>		61)2278205, 2278310 <u>at.com</u>						NANI NAROL	I, SURAT.		SHEET,ND:		REV,
									Surveyed by + K			-	-	RMAR (98241-74691) ey_kjp@yahoo.co	Location		CL FINAL SUBMISSION\VA	ASTAN GIPCL (TOPOGRAPHY S	SURVEY) FINAL 02.02.2022-MA	L.dwg	01	00



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PLUI.	AREA IN SQ.MT	HECTARE	DATE	12.01.2022	1CM.=25.0 MT.	Udhna, Surat-394 210 ph-(0261)2278205, 2278310 Mail ID : <u>unique@uniquesurat.com</u>			SHEET.ND:	REV,
NOGAMA	GAMA 983092.44 98.31					Surveyed by + K.J.Prmar (98241 74691)	Surveyed by :- K.J.PARMAR (98241 74691) Mail ID : <u>aonesurvey_kjp@yahoo.cc</u>	Location:- Gundle_3uprawar-2022/NDGAWA GPOL BOUNDARY CORDINATE/NDGAWA GIPOL/NDGAWA GIPOL FDWL SUBVISSION/GIPOL NAVI NAROLI NDGAWA SITEKTOPOGRAPHY SURVEY) -29012022 - FINAL MAIL	0 1.	00